## FAN5361

6MHz, 600mA / 750mA Synchronous Buck Regulator

## Features

■ 6MHz Fixed-Frequency Operation

- $35 \mu \mathrm{~A}$ Typical Quiescent Current
- Best-in-Class Load Transient Response
- Best-in-Class Efficiency

■ 600 mA or 750 mA Output Current Capability
■ 2.3 V to 5.5 V Input Voltage Range

- 1.0 to 1.90 V Fixed Output Voltage
- Low Ripple Light-Load PFM Mode
- Forced PWM and External Clock Synchronization
- Internal Soft-Start
- Input Under-Voltage Lockout (UVLO)

■ Thermal Shutdown and Overload Protection

- 6-bump WLCSP, 0.4 mm Pitch
- 6-pin $2 \times 2 \mathrm{~mm}$ UMLP


## Applications

- Cell Phones, Smart Phones
- Tablets, Netbooks ${ }^{\circledR}$, Ultra-Mobile PCs
- 3G, LTE, WiMAX ${ }^{\text {™ }}$, WiBro $^{\circledR}$, and $\mathrm{WiFi}^{\circledR}$ Data Cards
- Gaming Devices, Digital CamerasDC/DC Micro Modules


## Description

The FAN5361 is a 600 mA or 750 mA , step-down, switching voltage regulator that delivers a fixed output from a 2.3 V to 5.5 V input voltage supply. Using a proprietary architecture with synchronous rectification, the FAN5361 is capable of delivering a peak efficiency of $92 \%$, while maintaining efficiency over $80 \%$ at load currents as low as 1 mA .

The regulator operates at a nominal fixed frequency of 6 MHz , which reduces the value of the external components to 470 nH for the output inductor and $4.7 \mu \mathrm{~F}$ for the output capacitor. The PWM modulator can be synchronized to an external frequency source.
At moderate and light loads, pulse frequency modulation is used to operate the device in power-save mode with a typical quiescent current of $35 \mu \mathrm{~A}$. Even with such a low quiescent current, the part exhibits excellent transient response during large load swings. At higher loads, the system automatically switches to fixed-frequency control, operating at 6 MHz . In shutdown mode, the supply current drops below $1 \mu \mathrm{~A}$, reducing power consumption. For applications that require minimum ripple or fixed frequency, PFM mode can be disabled using the MODE pin.

The FAN5361 is available in 6-bump, 0.4 mm pitch, WaferLevel Chip-Scale Package (WLCSP) and a 6-lead $2 \times 2 \mathrm{~mm}$ ultra-thin MLP package (UMLP).

## Typical Applications



Figure 1. Typical Applications

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## Ordering Information

| Part Number | Output Voltage ${ }^{(1)}$ | Package | Temperature Range | Packing |
| :---: | :---: | :---: | :---: | :---: |
| FAN5361UC123X | 1.233 V | WLCSP-6, 0.4 mm Pitch | -40 to $+85^{\circ} \mathrm{C}$ | Tape and Reel |
| FAN5361UC182X | 1.820 V |  |  |  |
| FAN5361UC19X | 1.900 V |  |  |  |
| FAN5361UMP123X | 1.233 V | 6-Lead, $2 \times 2 \mathrm{~mm}$ UMLP |  |  |
| FAN5361UMP15X | 1.500 V |  |  |  |
| FAN5361UMP182X | 1.820 V |  |  |  |

## Note:

1. Other voltage options available on request. Contact a Fairchild representative.

## Pin Configurations



Figure 2. WLCSP, Bumps Facing Down
Figure 3. WLCSP, Bumps Facing Up


Figure 4. UMLP, Leads Facing Down

## Pin Definitions

| Pin \# |  | Name |  |
| :---: | :---: | :---: | :--- |
| WLCSP | UMLP |  |  |
| A1 | 3 | MODE | MODE. Logic 1 on this pin forces the IC to stay in PWM mode. A logic 0 allows the IC to <br> automatically switch to PFM during light loads. The regulator also synchronizes its switching <br> frequency to four times the frequency provided on this pin. Do not leave this pin floating. When <br> tying HIGH, use at least $1 \mathrm{k} \Omega$ series resistor if V IN is expected to exceed 4.5V. |
| B1 | 2 | SW | Switching Node. Connect to output inductor. |
| C1 | 1 | FB | Feedback / Vout. Connect to output voltage. |
| C2 | 6 | GND | Ground. Power and IC ground. All signals are referenced to this pin. |
| B2 | 5 | EN | Enable. The device is in shutdown mode when voltage to this pin is $<0.4 \mathrm{~V}$ and enabled when <br> $>1.2 \mathrm{~V}$. Do not leave this pin floating. When tying HIGH, use at least $1 \mathrm{k} \Omega$ series resistor if $\mathrm{V}_{\text {IN }}$ is <br> expected to exceed 4.5V. |
| A2 | 4 | VIN | Input Voltage. Connect to input power source. |

## Absolute Maximum Ratings

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

| Symbol |  | Parameter | Min. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| V IN | Input Voltage |  | -0.3 | 7.0 | V |
| $\mathrm{V}_{\text {Sw }}$ | Voltage on SW Pin |  | -0.3 | $\mathrm{V}_{\text {IN }}+0.3^{(2)}$ | V |
| $\mathrm{V}_{\text {CTRL }}$ | EN and MODE Pin Voltage |  | -0.3 | $\mathrm{V}_{\text {IN }}+0.3^{(2)}$ | V |
|  | Other Pins |  | -0.3 | $\mathrm{V}_{\text {IN }}+0.3^{(2)}$ | V |
| ESD | Electrostatic Discharge Protection Level | Human Body Model per JESD22-A114 | 4.0 |  | kV |
|  |  | Charged Device Model per JESD22-C101 |  | 5 |  |
| $\mathrm{T}_{J}$ | Junction Temperature |  | -40 | +150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {STG }}$ | Storage Temperature |  | -65 | +150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\mathrm{L}}$ | Lead Soldering Temperature, 10 Seconds |  |  | +260 | ${ }^{\circ} \mathrm{C}$ |

Note:
2. Lesser of 7 V or $\mathrm{V}_{\mathrm{IN}}+0.3 \mathrm{~V}$.

## Recommended Operating Conditions

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended operating conditions are specified to ensure optimal performance to the datasheet specifications. Fairchild does not recommend exceeding them or designing to Absolute Maximum Ratings.

| Symbol | Parameter | Min. | Typ. | Max. | Unit |
| :---: | :--- | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{CC}}$ | Supply Voltage Range | 2.3 |  | 5.5 | V |
| $\mathrm{I}_{\text {Out }}$ | Output Current | 0 |  | 600 | mA |
| L | Inductor |  | 0.47 |  | $\mu \mathrm{H}$ |
| $\mathrm{C}_{\text {IN }}$ | Input Capacitor |  | 2.2 |  | $\mu \mathrm{~F}$ |
| $\mathrm{C}_{\text {OUT }}$ | Output Capacitor | 1.6 | 4.7 | 12.0 | $\mu \mathrm{~F}$ |
| $\mathrm{~T}_{\mathrm{A}}$ | Operating Ambient Temperature | -40 |  | +85 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{J}$ | Operating Junction Temperature | -40 |  | +125 | ${ }^{\circ} \mathrm{C}$ |

## Thermal Properties

Junction-to-ambient thermal resistance is a function of application and board layout. This data is measured with four-layer 1s2p boards in accordance to JEDEC standard JESD51. Special attention must be paid not to exceed junction temperature $T_{J(\max )}$ at a given ambient temperate $\mathrm{T}_{\mathrm{A}}$.

| Symbol | Parameter |  | Typical | Unit |
| :---: | :---: | :--- | :---: | :---: |
| $\theta_{\mathrm{JA}}$ |  | Junction-to-Ambient Thermal Resistance | WLCSP | 150 |
|  |  | UMLP | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |  |

## Electrical Characteristics

Minimum and maximum values are at $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\text {EN }}=2.3 \mathrm{~V}$ to 5.5 V , $\mathrm{V}_{\text {MODE }}=0 \mathrm{~V}$ (AUTO Mode), $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$; circuit of Figure 1, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\text {IN }}=\mathrm{V}_{\mathrm{EN}}=3.6 \mathrm{~V}$.

| Symbol | Parameter | Conditions | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Power Supplies |  |  |  |  |  |  |
| $\mathrm{I}_{\mathrm{Q}}$ | Quiescent Current | No Load, Not Switching |  | 35 | 55 | $\mu \mathrm{A}$ |
|  |  | PWM Mode |  | 6 |  | mA |
| $\mathrm{I}_{(\mathrm{SD})}$ | Shutdown Supply Current | $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}, \mathrm{EN}=\mathrm{GND}$ |  | 0.05 | 1.00 | $\mu \mathrm{A}$ |
| V UVLO | Under-Voltage Lockout Threshold | Rising $\mathrm{V}_{\text {IN }}$ |  | 2.15 | 2.25 | V |
| $\mathrm{V}_{\text {UVHYST }}$ | Under-Voltage Lockout Hysteresis |  |  | 150 |  | mV |

Logic Inputs: EN and MODE Pins

| $\mathrm{V}_{\mathrm{IH}}$ | Enable HIGH-Level Input Voltage |  | 1.2 |  | V |
| :---: | :--- | :--- | :--- | :---: | :---: |
| $\mathrm{~V}_{\mathrm{IL}}$ | Enable LOW-Level Input Voltage |  |  |  | 0.4 |
| $\mathrm{~V}_{\text {LHYST }}$ | Logic Input Hysteresis Voltage |  |  | 100 | V |
| $\mathrm{I}_{\mathrm{IN}}$ | Enable Input Leakage Current | Pin to $\mathrm{V}_{\mathrm{IN}}$ or GND |  | 0.01 | 1.00 |

Switching and Synchronization

| $\mathrm{f}_{\mathrm{SW}}$ | Switching Frequency $^{(3)}$ | $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 5.4 | 6.0 | 6.6 | MHz |
| :---: | :--- | :--- | :---: | :---: | :---: | :---: |
| $\mathrm{f}_{\mathrm{SYNC}}$ | MODE Synchronization Range ${ }^{(3)}$ | Square Wave at MODE Input | 1.3 | 1.5 | 1.7 | MHz |

## Regulation

| $\mathrm{V}_{\mathrm{O}}$ | Output Voltage Accuracy | 1.900 V | $\mathrm{I}_{\text {LOAD }}=0$ to $750 \mathrm{~mA}^{(4)}$ | 1.832 | 1.900 | 1.957 | V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | PWM Mode ${ }^{(4)}$ | 1.832 | 1.900 | 1.938 |  |
|  |  | 1.820 V | $\mathrm{I}_{\text {LOAD }}=0$ to 600 mA | 1.784 | 1.820 | 1.875 |  |
|  |  |  | PWM Mode | 1.784 | 1.820 | 1.856 |  |
|  |  | 1.500 V | $\mathrm{I}_{\text {LOAD }}=0$ to 600 mA | 1.470 | 1.500 | 1.545 |  |
|  |  |  | PWM Mode | 1.470 | 1.500 | 1.530 |  |
|  |  | 1.233 V | $\mathrm{I}_{\text {LOAD }}=0$ to 600 mA | 1.207 | 1.233 | 1.272 |  |
|  |  |  | PWM Mode | 1.207 | 1.233 | 1.259 |  |
| $\mathrm{t}_{\text {ss }}$ | Soft-Start |  | From EN Rising Edge |  | 180 | 300 | $\mu \mathrm{s}$ |

## Output Driver

| $\mathrm{R}_{\mathrm{DS} \text { (on) }}$ | PMOS On Resistance | $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{GS}}=3.6 \mathrm{~V}$ |  | 350 |  | $\mathrm{m} \Omega$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NMOS On Resistance | $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{GS}}=3.6 \mathrm{~V}$ |  | 225 |  |  |
| ILIm(OL) | PMOS Open-Loop Peak Current Limit ${ }^{(5)}$ | $\mathrm{V}_{\text {OUT }}=1.233 \mathrm{~V}, 1.5 \mathrm{~V}, 1.82 \mathrm{~V}$ | 900 | 1100 | 1250 | mA |
|  |  | $\mathrm{V}_{\text {OUT }}=1.9 \mathrm{~V}$ | 1180 | 1375 | 1550 |  |
| $\mathrm{T}_{\text {TSD }}$ | Thermal Shutdown | CCM Only |  | 150 |  | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\mathrm{HYS}}$ | Thermal Shutdown Hysteresis |  |  | 15 |  | ${ }^{\circ} \mathrm{C}$ |

## Notes:

3. Limited by the effect of toff minimum (see Figure 14 and Figure 15 in Typical Performance Characteristics).
4. Output voltage accuracy minimum: 1.862 V for $\mathrm{V}_{\mathrm{IN}} 2.7$ to 5.5 V on 1.9 V option.
5. Refer to Operation Description and Typical Characteristics for closed-loop data.

## Typical Performance Characteristics

Unless otherwise noted, $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{EN}}=3.6 \mathrm{~V}, \mathrm{~V}_{\text {MODE }}=0 \mathrm{~V}$ (AUTO Mode), $\mathrm{V}_{\mathrm{OUT}}=1.82 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.


Figure 5. Efficiency vs. Load Current and Input Supply Figure 6. Efficiency vs. Load Current and Temperature


Figure 7. $1.233 V_{\text {out }}$ Efficiency vs. Load Current and Supply


Figure 9. Load Regulation


Figure 8. Efficiency, Auto PWM/PFM vs. Forced PWM


Figure 10. 1.233V ${ }_{\text {out }}$ Load Regulation vs. Input Supply

## Typical Performance Characteristics (Continued)

Unless otherwise noted, $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{EN}}=3.6 \mathrm{~V}, \mathrm{~V}_{\text {MODE }}=0 \mathrm{~V}$ ( AUTO Mode), $\mathrm{V}_{\mathrm{OUT}}=1.82 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.


Figure 11. Load Regulation, Auto PFM / PWM and Forced PWM


Figure 13. 1.233V Vut $_{\text {оut }}$ Peak-to-Peak Output Voltage Ripple


Figure 15. $1.233 \mathrm{~V}_{\text {оut }}$ Effect of $\mathrm{t}_{\text {Off(MIN) }}$ on Reducing Switching Frequency


Figure 12. 1.82V ${ }_{\text {out }}$ Peak-to-Peak Output Voltage Ripple


Figure 14. Effect of $\mathrm{t}_{\mathrm{off}(\mathrm{MIN})}$ on Reducing Switching Frequency


Figure 16. PFM / PWM Boundaries

## Typical Performance Characteristics (Continued)

Unless otherwise noted, $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{EN}}=3.6 \mathrm{~V}, \mathrm{~V}_{\text {MODE }}=0 \mathrm{~V}$ ( AUTO Mode), $\mathrm{V}_{\mathrm{OUT}}=1.82 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.


Figure 17. 1.233V ${ }_{\text {out }}$ PFM / PWM Boundaries


Figure 18. Quiescent Current vs. Input Voltage


Figure 19. Shutdown Current vs. Temperature

## Typical Performance Characteristics (Continued)

Unless otherwise noted, $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{EN}}=3.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{MODE}}=0 \mathrm{~V}$ (AUTO Mode), $\mathrm{V}_{\mathrm{OUT}}=1.82 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, 5 \mu \mathrm{~s} /$ div. horizontal sweep.


Figure 20. Line Transient $3.3 \mathrm{~V}_{\text {IN }}$ to $3.9 \mathrm{~V}_{\text {IN }}$, 50mA Load, 10 $10 \mathrm{~s} / \mathrm{div}$.

Figure 21. Line Transient $3.3 \mathrm{~V}_{\text {IN }}$ to $3.9 \mathrm{~V}_{\text {IN }}$, 250mA Load, $10 \mu \mathrm{~s} / \mathrm{div}$.


Figure 22. Combined Line/Load Transient 3.9 to $3.3 \mathrm{~V}_{\text {IN }}$ Combined with 40 mA to 400 mA Load Transient

Figure 23. Combined Line/Load Transient 3.3 to $3.9 \mathrm{~V}_{\text {IN }}$ Combined with 400 mA to 40 mA Load Transient


Figure 24. Load Transient 0 to $150 \mathrm{~mA}, 2.5 \mathrm{~V}_{\mathrm{IN}}$
Figure 25. Load Transient 50 to $250 \mathrm{~mA}, 2.5 \mathrm{~V}$ IN

## Typical Performance Characteristics (Continued)

Unless otherwise noted, $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{EN}}=3.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{MODE}}=0 \mathrm{~V}$ (AUTO Mode), $\mathrm{V}_{\mathrm{OUT}}=1.82 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, 5 \mu \mathrm{~s} /$ div. horizontal sweep.


Figure 26. Load Transient 150 to $\mathbf{4 0 0 m A}, 2.5 \mathrm{~V}$ IN


Figure 28. Load Transient 50 to $\mathbf{2 5 0 m A}, \mathbf{3 . 6} \mathrm{V}_{\mathrm{IN}}$


Figure 30. Load Transient 0 to $150 \mathrm{~mA}, 4.5 \mathrm{~V}_{\mathrm{IN}}$
Figure 27. Load Transient 0 to $150 \mathrm{~mA}, 3.6 \mathrm{~V}$ IN



Figure 32. Load Transient 150 to $400 \mathrm{~mA}, 4.5 \mathrm{~V}$ IN

## Typical Performance Characteristics (Continued)

Unless otherwise noted, $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{EN}}=3.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{MODE}}=0 \mathrm{~V}$ (AUTO Mode), $\mathrm{V}_{\mathrm{OUT}}=1.82 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, 5 \mu \mathrm{~s} / \mathrm{div}$. horizontal sweep.


Figure 33. Metallic Short Applied at $\mathrm{V}_{\mathrm{out}}, \mathbf{5 0 \mu s} / \mathrm{div}$.
Figure 34. Metallic Short Applied at Vout


Figure 35. Over-Current Fault Response, $R_{\text {LOAD }}=1 \Omega, 50 \mu \mathrm{~s} / \mathrm{div}$.


Figure 36. Over-Current Fault Response, $\mathrm{R}_{\text {LOAD }}=1 \Omega$


Figure 38. Soft-Start, $R_{\text {LOAD }}=50 \Omega, 20 \mu \mathrm{~s} / \mathrm{div}$.

## Typical Performance Characteristics (Continued)

Unless otherwise noted, $\mathrm{V}_{\mathbb{I N}}=\mathrm{V}_{\mathrm{EN}}=3.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{MODE}}=0 \mathrm{~V}$ (AUTO Mode), $\mathrm{V}_{\text {OUT }}=1.82 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.



Figure 40. Power Supply Rejection Ratio at $\mathbf{3 0 0} \mathrm{mA}$ Load

## Operation Description

The FAN5361 is a 600 mA or 750 mA , step-down, switching voltage regulator that delivers a fixed output from an input voltage supply of 2.3 V to 5.5 V . Using a proprietary architecture with synchronous rectification, the FAN5361 is capable of delivering a peak efficiency of $92 \%$, while maintaining efficiency over $80 \%$ at load currents as low as 1 mA . The regulator operates at a nominal frequency of 6 MHz at full load, which reduces the value of the external components to 470 nH for the inductor and $4.7 \mu \mathrm{~F}$ for the output capacitor.

## Control Scheme

The FAN5361 uses a proprietary, non-linear, fixed-frequency PWM modulator to deliver a fast load transient response, while maintaining a constant switching frequency over a wide range of operating conditions. The regulator performance is independent of the output capacitor ESR, allowing for the use of ceramic output capacitors. Although this type of operation normally results in a switching frequency that varies with input voltage and load current, an internal frequency loop holds the switching frequency constant over a large range of input voltages and load currents.

For very light loads, the FAN5361 operates in discontinuous current (DCM) single-pulse PFM mode, which produces low output ripple compared with other PFM architectures. Transition between PWM and PFM is seamless, with a glitch of less than 18 mV at $\mathrm{V}_{\text {out }}$ during the transition between DCM and CCM modes.

Combined with exceptional transient response characteristics, the very low quiescent current of the controller ( $35 \mu \mathrm{~A}$ ) maintains high efficiency; even at very light loads, while preserving fast transient response for applications requiring tight output regulation.

## Enable and Soft-Start

When EN is LOW, all circuits in FAN5361 are off and the IC draws $\sim 50 \mathrm{nA}$ of current. When EN is HIGH and $\mathrm{V}_{\mathrm{IN}}$ is above its UVLO threshold, the regulator begins a soft-start cycle. The output ramp during soft-start is a fixed slew rate of $50 \mathrm{mV} / \mu \mathrm{s}$ from 0 to $1 \mathrm{~V}_{\text {Out }}$, then $12.5 \mathrm{mV} / \mu \mathrm{s}$ until the output reaches its setpoint. Regardless of the state of the MODE pin, PFM mode is enabled to prevent current from being discharged from Cout if soft-start begins when Cout is charged.

The IC may fail to start if heavy load is applied during startup and/or if excessive Cout is used. This is due to the currentlimit fault response, which protects the IC in the event of an over-current condition present during soft-start.
The current required to charge $\mathrm{C}_{\text {out }}$ during soft-start is commonly referred to as "displacement current" is given as:

$$
\begin{equation*}
\mathrm{I}_{\mathrm{DISP}}=\mathrm{C}_{\text {OUT }} \cdot \frac{\mathrm{dV}}{\mathrm{dt}} \tag{1}
\end{equation*}
$$

where the $\frac{d V}{d t}$ term refers to the soft-start slew rate above.

To prevent shut-down during soft-start, the following condition must be met:

$$
\begin{equation*}
\mathrm{I}_{\mathrm{DISP}}+\mathrm{I}_{\mathrm{LOAD}}<\mathrm{I}_{\mathrm{MAX}(\mathrm{DC})} \tag{2}
\end{equation*}
$$

where $I_{\operatorname{MAX}(D C)}$ is the maximum load current the IC is guaranteed to support ( 600 mA or 750 mA ).
Table 1 shows combinations of $\mathrm{C}_{\text {OUt }}$ that allow the IC to start successfully with the minimum R ROAD that can be supported.

Table 1. Minimum Rload Values for Soft-Start with Various Cout Values

| Cout | Minimum $\mathrm{R}_{\text {Load }}$ |
| :---: | :---: |
| $4.7 \mu \mathrm{~F}, 0402$ | $V_{\text {OUt }} / 0.60$ |
| $2 \times 4.7 \mu \mathrm{~F}, 0402$ | Vout / 0.60 |
| $10 \mu \mathrm{~F}, 0603$ | Vout / 0.60 |
| 10رF, 0805 | Vout / 0.50 |

## Startup into Large Cout

Multiple soft-start cycles are required for no-load startup if $C_{\text {out }}$ is greater than $15 \mu \mathrm{~F}$. Large Cout requires light initial load to ensure the FAN5361 starts appropriately. The IC shuts down for $85 \mu$ s when I IISP exceeds I LIMIT for more than $21 \mu \mathrm{~s}$ of current limit. The IC then begins a new soft-start cycle. Since Cout retains its charge when the IC is off, the IC reaches regulation after multiple soft-start attempts.

## MODE Pin

Logic 1 on this pin forces the IC to stay in PWM mode. A logic 0 allows the IC to automatically switch to PFM during light loads. If the MODE pin is toggled, the converter synchronizes its switching frequency to four times the frequency on the mode pin ( $f_{\text {MODE }}$ ).

The MODE pin is internally buffered with a Schmitt trigger, which allows the MODE pin to be driven with slow rise and fall times. An asymmetric duty cycle for frequency synchronization is also permitted as long as the minimum time below $\mathrm{V}_{\mathrm{IL}(\operatorname{MAX})}$ or above $\mathrm{V}_{\mathrm{IH}(\mathrm{MAX})}$ is 100 ns .

## Current Limit, Fault Shutdown, and Restart

A heavy load or short circuit on the output causes the current in the inductor to increase until a maximum current threshold is reached in the high-side switch. Upon reaching this point, the high-side switch turns off, preventing high currents from causing damage. The regulator continues to limit the current cycle-by-cycle. After $21 \mu \mathrm{~s}$ of current limit, the regulator triggers an over-current fault, causing the regulator to shut down for about $85 \mu$ s before attempting a restart.

If the fault was caused by short circuit, the soft-start circuit attempts to restart and produces an over-current fault after about $32 \mu \mathrm{~s}$, which results in a duty cycle of less than $30 \%$, limiting power dissipation.
The closed-loop peak-current limit, $\mathrm{I}_{\mathrm{LIM}(\mathrm{PK})}$, is not the same as the open-loop tested current limit, llim(ol), in the Electrical Characteristics table. This is primarily due to the effect of propagation delays of the IC current limit comparator.

## Under-Voltage Lockout (UVLO)

When EN is HIGH, the under-voltage lockout keeps the part from operating until the input supply voltage rises high enough to properly operate. This ensures no misbehavior of the regulator during startup or shutdown.

## Thermal Shutdown (TSD)

When the die temperature increases, due to a high load condition and/or a high ambient temperature, the output switching is disabled until the temperature on the die has fallen sufficiently. The junction temperature at which the thermal shutdown activates is nominally $150^{\circ} \mathrm{C}$ with a $15^{\circ} \mathrm{C}$ hysteresis.

## Minimum Off-Time Effect on Switching Frequency

$t_{\text {off(Min) }}$ is 50 ns . This imposes constraints on the maximum $\frac{V_{\text {OUT }}}{V_{\text {IN }}}$ that the FAN5361 can provide, or the maximum output voltage it can provide at low $\mathrm{V}_{\mathbb{I N}}$ while maintaining a fixed switching frequency in PWM mode.

When $V_{\text {IN }}$ is LOW, fixed switching is maintained as long as $\frac{V_{O U T}}{V_{I N}} \leq 1-t_{O F F(M I N)} \bullet f_{S W} \approx 0.7$.

The switching frequency drops when the regulator cannot provide sufficient duty cycle at 6 MHz to maintain regulation. This occurs when Vout is greater than or equal to 1.82 V and $\mathrm{V}_{\mathrm{IN}}$ is below 2.9 V at high load currents (see Figure 15).
The calculation for switching frequency is given by:
$f_{S W}=\min \left(\frac{1}{t_{S W(M A X)}}, 6 M H z\right)$
where:

$$
\begin{equation*}
t_{S W(M A X)}=50 n s \cdot\left(1+\frac{V_{\text {OUT }}+I_{\text {OUT }} \bullet R_{\text {OFF }}}{V_{I N}-I_{O U T} \bullet R_{O N}-V_{O U T}}\right) \tag{4}
\end{equation*}
$$

where:

$$
\begin{aligned}
& R_{\text {OFF }}=R_{\text {DSON_N }}+D C R_{L} \\
& R_{\text {ON }}=R_{D S O N_{-} P}+D C R_{L}
\end{aligned}
$$

## Applications Information

## Selecting the Inductor

The output inductor must meet both the required inductance and the energy handling capability of the application. The inductor value affects average current limit, the PWM-toPFM transition point, output voltage ripple, and efficiency.

The ripple current $(\Delta I)$ of the regulator is:

$$
\begin{equation*}
\Delta I \approx \frac{V_{O U T}}{V_{I N}} \cdot\left(\frac{V_{I N}-V_{O U T}}{L \bullet f_{S W}}\right) \tag{5}
\end{equation*}
$$

The maximum average load current, $\mathrm{I}_{\mathrm{MAX}(\text { LOAD }), ~ i s ~ r e l a t e d ~ t o ~}$ the peak current limit, $\mathrm{I}_{\mathrm{LIM(PK)}}$ by the ripple current, given by:

$$
\begin{equation*}
I_{\operatorname{MAX}(\mathrm{LOAD})}=\mathrm{I}_{\mathrm{LIM}(\mathrm{PK})}-\frac{\Delta \mathrm{l}}{2} \tag{6}
\end{equation*}
$$

The transition between PFM and PWM operation is determined by the point at which the inductor valley current crosses zero. The regulator DC current when the inductor current crosses zero, $\mathrm{I}_{\mathrm{DCM}}$, is:

$$
\begin{equation*}
\mathrm{I}_{\mathrm{DCM}}=\frac{\Delta \mathrm{l}}{2} \tag{7}
\end{equation*}
$$

The FAN5361 is optimized for operation with $L=470 \mathrm{nH}$, but is stable with inductances up to $1.2 \mu \mathrm{H}$ (nominal). Up to $2.2 \mu \mathrm{H}$ (nominal) may be used; however, in that case, $\mathrm{V}_{\mathrm{IN}}$ must be greater than or equal to 2.7 V . The inductor should be rated to maintain at least $80 \%$ of its value at $\mathrm{I}_{\text {LIM(PK) }}$.

Efficiency is affected by the inductor DCR and inductance value. Decreasing the inductor value for a given physical size typically decreases the DCR; but since $\Delta l$ increases, the RMS current increases, as do the core and skin effect losses.

$$
\begin{equation*}
I_{\mathrm{RMS}}=\sqrt{\mathrm{I}_{\mathrm{OUT}(\mathrm{DC})^{2}+\frac{\Delta \mathrm{I}^{2}}{12}} \text {. }} \tag{8}
\end{equation*}
$$

The increased RMS current produces higher losses through the $R_{D S(O N)}$ of the IC MOSFETs, as well as the inductor DCR.
Increasing the inductor value produces lower RMS currents, but degrades transient response. For a given physical inductor size, increased inductance usually results in an inductor with lower saturation current and higher DCR.

Table 2 shows the effects of inductance higher or lower than the recommended 470nH on regulator performance.

## Output Capacitor

Table 3 suggests 0402 capacitors. 0603 capacitors may further improve performance in that the effective capacitance is higher. This improves transient response and output ripple.

Increasing Cout has no effect on loop stability and can therefore be increased to reduce output voltage ripple or to improve transient response. Output voltage ripple, $\Delta \mathrm{V}_{\text {OUT }}$, is:

$$
\begin{equation*}
\Delta V_{\text {OUT }}=\Delta l \bullet\left(\frac{1}{8 \bullet C_{\text {OUT }} \bullet f_{S W}}+E S R\right) \tag{9}
\end{equation*}
$$

## Input Capacitor

The $2.2 \mu \mathrm{~F}$ ceramic input capacitor should be placed as close as possible between the VIN pin and GND to minimize the parasitic inductance. If a long wire is used to bring power to the IC, additional "bulk" capacitance (electrolytic or tantalum) should be placed between $\mathrm{C}_{\mathrm{IN}}$ and the power source lead to reduce ringing that can occur between the inductance of the power source leads and $\mathrm{C}_{\mathrm{IN}}$.
The effective capacitance value decreases as $\mathrm{V}_{\mathrm{IN}}$ increases due to DC bias effects.

Table 2. Effects of Changes in Inductor Value (from 470nH Recommended Value) on Regulator Performance

| Inductor Value | $\mathbf{I}_{\text {MAX(LOAD) }}$ | $\Delta \mathbf{V}_{\text {OUT }}$ | Transient Response |
| :---: | :---: | :---: | :---: |
| Increase | Increase | Decrease | Degraded |
| Decrease | Decrease | Increase | Improved |

Table 3. Recommended Passive Components and their Variation Due to DC Bias

| Component | Description | Vendor | Min. | Typ. | Max. ${ }^{(6)}$ | Comment |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $470 \mathrm{nH}, 2012$, <br> $90 \mathrm{~m} \Omega, 1.1 \mathrm{~A}$ | Murata LQM21PNR47MC0 <br> Murata LQM21PNR54MG0 <br> Hitachi Metals HSLI-201210AG-R47 | 300 nH | 470 nH | 520 nH | Minimum value occurs <br> at maximum current |
| $\mathrm{C}_{\mathrm{IN}}$ | $2.2 \mu \mathrm{~F}, 6.3 \mathrm{~V}$, <br> X5R, 0402 | Murata or Equivalent <br> GRM155R60J225ME15 <br> GRM188R60J225KE19D | $1.0 \mu \mathrm{~F}$ | $2.2 \mu \mathrm{~F}$ | $2.4 \mu \mathrm{~F}$ | Decrease primarily due <br> to DC bias (VIN) and <br> elevated temperature |
| $\mathrm{C}_{\text {Out }}$ | $4.7 \mu \mathrm{~F}, \mathrm{X} 5 R$, <br> 0402 | Murata or Equivalent GRM155R60G475M <br> GRM155R60E475ME760 | $1.6 \mu \mathrm{~F}$ | $4.7 \mu \mathrm{~F}$ | $5.2 \mu \mathrm{~F}$ | Decrease primarily due <br> to DC bias (Vout) |

## Note:

6. Higher inductance values are also acceptable. See "Selecting the Inductor" instructions in Applications Information.

## PCB Layout Guidelines

There are only three external components: the inductor and the input and output capacitors. For any buck switcher IC, including the FAN5361, it is important to place a low-ESR input capacitor very close to the IC, as shown in Figure 41. The input capacitor ensures good input decoupling, which helps reduce noise appearing at the output terminals and ensures that the control sections of the IC do not behave
erratically due to excessive noise. This reduces switching cycle jitter and ensures good overall performance. It is important to place the common GND of $\mathrm{C}_{\mathrm{IN}}$ and $\mathrm{C}_{\text {out }}$ as close as possible to the FAN5361 C2 terminal. There is some flexibility in moving the inductor further away from the IC; in that case, $\mathrm{V}_{\text {Out }}$ should be considered at the Cout terminal.


Figure 41. PCB Layout Guidance

## Physical Dimensions



Figure 42. 6-Bump WLCSP, 0.4 mm Pitch

## Product-Specific Dimensions

| Product | $\mathbf{D}$ | $\mathbf{E}$ | $\mathbf{X}$ | $\mathbf{Y}$ |
| :---: | :---: | :---: | :---: | :---: |
| FAN5361UCX | $1.370+/-0.040$ | $0.970+/-0.040$ | 0.285 | 0.285 |

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## Physical Dimensions



Figure 43. 6-Lead, $2 \times 2 \mathrm{~mm}$, Ultra-Thin Molded Leadless Package (UMLP)

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| $\overbrace{}^{(8)}$ | MicroPak ${ }^{\text {™ }}$ | SuperFET ${ }^{\text {® }}$ | ${ }^{\mu}{ }^{\text {SerDes }}$ |
| Fairchild ${ }^{\text {® }}$ | MicroPak2 ${ }^{\text {mim }}$ | SuperSOT ${ }^{\text {m/3 }} 3$ | SerDes |
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